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1 ELECTROMECHANICAL DRIVE ELEMENT COMPRISING
2 A PIEZOELECTRIC ELEMENT

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4 ELECTROMECHANICAL DRIVE ELEMENT

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6 Description

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8 The invention concerns an electromechanical drive element, in particular for the
9 exact positioning of an object in the nanometer to centimeter range, comprising a
10 rotor supported in a bearing element and at least one piezoelectric element that
11 can be acted upon with an electric voltage.

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13 EP 0 611 485 B1 makes known a linear motor comprising a piezoelectric element
14 that is suited to positioning a tip of a needle-like probe down to a range of the
15 atomic order on a surface of an object. This known positioning element is
16 unusual in that the probes can move with high precision in the nanometer range
17 while, at the same time, travelling greater adjusting paths in the centimeter
18 range. As such, it avoids the disadvantages of traditional devices such as guide
19 play, reversing play, drift, susceptibility to vibration, or oversizing.

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21 The known positioning element is only conditionally suited to changing the
22 angular position of an object, however. To accomplish this, the positioning
23 elements must be used with corresponding coupling elements to the object to be
24 positioned, such as a probe. Additionally, only small angular adjustments can be
25 achieved.

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27 The present invention is based on the object of creating an electromechanical
28 drive element that can adjust the angular position of objects with high precision
29 using minimal structural expenditure.

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1 The object is solved according to the invention using an electromechanical drive
2 element of the type described initially in that the bearing element has at least one
3 rotor receptacle supported on a bearing block in a fashion that allows it to rotate
4 with limits, which rotor receptacle can be rotated by the expansion and/or
5 contraction—induced by an electric voltage—of the at least one piezoelectric
6 element.

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8 The drive element according to the invention can be produced in very small
9 dimensions, so that disruptions by temperature or external mechanical effects
10 such as impact sounds are extremely minimal.

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12 The at least one piezoelectric element changes its expansion under the influence
13 of the electric voltage by approximately only one micrometer, so that the motions
14 of the at least one rotor receptacle are extremely minimal. So that the rotor can
15 also travel greater adjusting paths, the rotor can be supported in the at least one
16 rotor receptacle in a manner that allows it to rotate with friction. The friction
17 between the rotor and the at least one rotor receptacle can thereby preferably be
18 such that the rotor does not follow relatively rapid revolutions of the at least one
19 rotor receptacle, but follows relatively slow revolutions of the at least one rotor
20 receptacle. Therefore, if the rotor receptacle is moved slowly by the piezoelectric
21 element, the rotor follows the motion. If, on the other hand, the rotor receptacle is
22 moved relatively quickly by the piezoelectric element, the rotor can no longer
23 follow the motion due to its inertia. Using successive, alternating slow and rapid
24 motions of the rotor receptacle, a quasi continuous revolution of the rotor in the
25 rotor receptacle can be achieved. The electrodes of the at least one piezoelectric
26 element can be connected to a saw-tooth voltage generator for this purpose,
27 which generates alternating slow and rapid expansions and contractions of the at
28 least one piezoelectric element and, therefore, revolutions of the at least one
29 rotor receptacle, whereby the rotor follows the slow revolutions and does not
30 follow the rapid revolutions.

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1 Preferably the at least one rotor receptacle can be a bearing ring that is
2 supported on the bearing block by way of multiple fixed members. The fixed
3 members form flectors, which gives the element high mechanical stability. In
4 traditional arrangements, forces transferred to the piezoelectric element from the
5 outside, in particular forces transverse to its direction of expansion, can destroy
6 the fragile piezoelectric crystal. The flectors formed by the fixed members can
7 absorb such transverse forces, however, so that the piezoelectric crystal is not
8 destroyed.

9

10 A further advantage of this arrangement lies in the fact that the flectors do not
11 need to guide the parts to be moved and thereby generate restoring forces. The
12 restoring forces of the fixed members only act upon the piezoelectric element
13 and are also very small, because the piezoelectric element expands or contracts
14 by approximately only one micrometer. Since the fixed members do not grip the
15 rotor, arbitrarily big angular adjustments of the rotor can be achieved as well.

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17 In a further advantageous design, the bearing element can have two bearing
18 rings as rotor receptacles supported on bearing blocks by way of multiple fixed
19 members in which the ends of the rotor are supported, whereby at least one of
20 the bearing rings can be rotated by means of at least one piezoelectric element.
21 It is therefore also possible to drive the rotor from both sides or from one side
22 only, whereby the second bearing ring then serves as a pure abutment. In every
23 case, the two bearing rings form two friction bearings that are pressed against
24 the rotor, which makes it possible for the rotor to rotate without play. Precise
25 adjustments in the nanometer range can also be achieved as a result.

26

27 In another design, the bearing element can have a piezoelectrically driven
28 bearing ring for accommodating one end of the rotor and a lower-friction
29 abutment for the other end of the rotor. Particularly precise motions can be
30 achieved using such a design.

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1 To reduce the friction, the rotor can also have tapering ends. They can be
2 designed as spherical cups, for example. If the rotor is driven on only one side, it
3 is advantageous if the spherical cup on the abutment has a smaller diameter.

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5 A preferred embodiment of a drive element according to the invention will be
6 described below in greater detail using the diagram.

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8 Figure 1 shows a side view of a drive element according to the invention.

9 Figure 2 shows an internal view of a bearing element of the drive element from
10 Figure 1.

11

12 The drive element 10 from Figure 1 has a rotor 11 with tapering ends 11.1 and
13 11.2 that are supported in two bearing elements 12 and 13. The two bearing
14 elements 12 and 13 are connected with each other by way of braces 14.
15 Together they form the bearing element for the rotor 11. The bearing elements
16 12 and 13 are thereby pressed against the rotor in springy fashion.

17

18 In the internal view of the bearing element 12 from Figure 2 it is obvious that it is
19 formed from a bearing block 15, to which a bearing ring 16 is fastened as rotor
20 receptacle by way of three fixed members 17. The rotor 11, which is not shown in
21 Figure 2, is then inserted in the bearing ring 16. Using a piezoelectric element 18,
22 the electrodes of which are connected with a saw-tooth voltage generator, for
23 example, in a fashion not shown in greater detail, the bearing ring 16 can be set
24 into rotation by expansion and contraction of the piezoelectric element 18,
25 whereby the fixed elements 17 act as deflectors. The rotor 11 is supported in the
26 bearing ring 16 with friction in such a fashion that it can follow slow revolutions of
27 the bearing ring 16, but cannot follow rapid motions due to its inertia. Using slow
28 motions of the bearing ring 16, the rotor can therefore be adjusted in very small
29 angular adjustments, while large angular adjustments or even a continuous
30 revolution of the rotor 11 can be achieved by alternating between rapid and slow
31 motions of the bearing ring 16.

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2 The drive element 10 shown is therefore suited to positioning an object with very
3 small angular adjustments as well as with large angular adjustments.

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5 The second bearing element 13 can be designed exactly the same as the
6 bearing element 12, but it can also form a simple abutment for the rotor,
7 whereby, advantageously, the friction between the rotor 11 and the abutment 13
8 is less than between the rotor 11 and the bearing ring 16.

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